



Performance of SIFCON with Steel Slag

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Abstract

Slurry infiltrated fibrous concrete (SIFCON) is a new and unique type of high performance concrete invented by Lankard in 1979, containing high percentage of fiber about 6% to 20% by volume. SIFCON possesses high strength as well as large ductility and has excellent potential for structural application. The matrix in SIFCON has no coarse aggregate but high cementitious content. The aim of study is to evaluate the performance of SIFCON mortar with lower fiber percentage and to minimize the fine aggregate usage by replacing it with industrial waste i.e. steel slag. Thereby, it also helps in effective disposal of industrial waste and helps in mitigating environmental pollution. The main objective of this study is to determine the effect of partial replacement of sand with steel slag on the mechanical properties of SIFCON mortar. The experimental program was carried out with 2%, 3% and 4% of fiber content by volume combined with replacement of sand by steel slag in proportion of 10% and 20% by weight. For this purpose, compressive strength, flexural strength, split tension and impact strength of SIFCON specimens were tested after 7 and 28 days of curing, yielding positive results.

1 Introduction

Slurry Infiltrated Fibrous CONcrete (SIFCON used herein after) is a fibrous concrete having high fiber content infiltrated with either cement slurry or cement mortar. SIFCON is a high performance concrete less than half a century old. Owing to the lesser time elapsed since its invention, very less research work has been performed to evaluate it on the grounds of durability and cost control. SIFCON possesses high toughness and impact resistance thereby rendering it suitable for blast resistant and impact resistant structures. Not only this, it can also be used as a good seismic retrofitting option. SIFCON is a concrete rich in cement matrix and fibrous content thus eliminating

the coarse fraction. Elimination of coarser fraction and inclusion of large volume of fiber is a major difference between SIFCON and Fiber reinforced concrete (FRC). The amount of fibers required in normal FRC is less than 2%, whereas in SIFCON the volume of fibers ranges from 6% to 20%. The large quantity of fiber and cement increases the overall production and placement cost of SIFCON, thus reducing its use. In past, attempts have been made to reduce the cement content but keeping the binder phase intact, by replacing cement with mineral admixtures such as fly ash, silica fumes etc. In this study, the amount of fibers has been restricted to 2%, 3% and 4% of volume of concrete. Furthermore, the sand has been partially replaced by ground Steel slag (referred to as Steel slag sand) obtained from steel industry. Slag is a byproduct obtained from steel furnace. Its handling and disposal has long been a source of distress for steel industry, moreover it's highly detrimental for environment as well. This slag is an inert, strong and hard material which can be suitably used in construction industry. To be used, it can be crushed to finer fraction from its large sized boulders in replacement of river sand in conventional and high performance concrete. Fig. 1 shows the variations in the sizes of the steel slag. In the present study SIFCON specimens were prepared for compression, flexural and impact tests and evaluated after 7 and 28 days of curing under normal temperature and test conditions.

2 Material used

The materials used for this study conforms to the Indian standards. After analyzing the previous experiments conducted on SIFCON, materials with following specifications were used.

- *Cement*: OPC 53 Grade Cement of fineness 2% Specific Gravity 3.10, Standard Consistency 35%, IST and FST 35 and 480 minutes respectively.
- *Fiber*: Hook ended steel fibers of aspect ratio 60 and length 35 mm.
- *Sand*: Locally available River Sand passing through 2.00 mm and retained on 0.075 mm sieve.
- *Steel slag*: Steel Slag from nearby steel manufacturing plant of specific gravity 2.89, water absorption 12.21%, passing through 2.00 mm and retained on 0.075 mm.
- *Water*: Locally available drinking water was used for mixing and curing of specimens.

The properties of materials used are given in Table 1 and Table 2.



Figure 1 : Various sizes of steel slag available

Ordinary Portland Cement (OPC 53)	
Standard Consistency (%)	35
Initial Setting time (Min)	35
Final Setting time (Min)	480
Fineness (%)	2
Natural sand	
Fineness Modules	2.9
Water Absorption (%)	1.42
Specific gravity	2.7
Silt content (%)	3
Density (kg/m ³)	1490
Steel Slag	
Fineness Modules	2.95
Water Absorption (%)	12.21
Specific gravity	2.89
Silt content (%)	1
Density (kg/m ³)	2140
Color	Dark Black
10% Steel slag and 90% Natural sand	
Fineness Modules	2.87
20% Steel slag and 80% Natural sand	
Fineness Modules	2.68

Table 1: Physical Properties of material used

Content	Steel Slag (%)	Cement OPC (%)
CaO	41.69	64.2
SiO ₂	33.82	22.0
T-Fe	0.42	3.0
MgO	7.40	1.5
Al ₂ O ₃	13.39	5.5
S	0.81	2.0
P ₂ O ₅	<0.1	-
MnO	0.3	-

Table 2: Chemical composition of material used

3 Mix proportions

The matrix in SIFCON has no coarse aggregates, but a high cementitious content. There is no specific method for mix design of SIFCON. Generally the proportion of cement and sand used in SIFCON are 1:1, 1:1.5 or 1:2. For this study, cement and sand were mixed in a proportion of 1:1, with a water cement ratio of 0.40.

The specimens were cast with fiber content of 2%, 3% and 4% by volume fraction and by replacing sand with steel slag in proportion of 10% and 20% by weight and the obtained results were compared with control mix i.e. 100% natural sand specimens. Mix proportion for different percentage replacement of steel slag sand in SIFCON is given in Table 3.

Number	Mix proportion	Replacement Level (%)	W/C ratio	Material requirement (kg/m ³)				
				Water	Cement	Sand	Steel slag	Fiber
SIFCON 2	1:1	0	0.40	285.71	714.28	714.28	0	157
	1:1	10	0.40	285.71	714.28	642.85	71.42	157
	1:1	20	0.40	285.71	714.28	571.42	142.85	157
SIFCON 3	1:1	0	0.40	285.71	714.28	714.28	0	235.50
	1:1	10	0.40	285.71	714.28	642.85	71.42	235.50
	1:1	20	0.40	285.71	714.28	570.42	142.85	235.50
SIFCON 4	1:1	0	0.40	285.71	714.28	714.28	0	314
	1:1	10	0.40	285.71	714.28	642.85	71.42	314
	1:1	20	0.40	285.71	714.28	571.42	142.85	314

Table 3: Mix Proportion

4 Procedure for casting specimen

Due to extremely high fiber content in SIFCON the mixing of steel fibers becomes a difficult task and it cannot be mixed as easily as in the case of FRC. So a special method for the SIFCON production has been used for this study. Dry mixing of weighted cement and sand is done meticulously in a pan. Water is added in the dry mix corresponding to water-cement ratio of 0.40. Water is to be added in parts. First, a thin layer of mortar with fluid consistency is placed at the bottom of the previously lubricated mould. Next, a layer of steel fiber is placed on the preplaced slurry. Again, slurry is infiltrated on to steel fiber layer and proper compaction is done by hand tamping. The entire mould is filled with alternate layers of slurry and steel fibers followed by surface finishing. The specimens were mixed compacted and cast carefully by following this procedure. The specimens were demoulded after 24 hours and cured for 7 and 28 days.

5 Test Program

The test program consisted of testing three specimens per test, each for 7 and 28 day. The sand was replaced with steel slag in the proportion of 10% and 20% by weight, keeping the proportions of other constituents constant. The specimen results were compared with control SIFCON specimens. The details of the tests conducted on fresh and hardened SIFCON specimens are as follows:

5.1 Flow Test

To check the Fluidity, viscosity and filling ability without bleeding and segregation of cement mortar, Slump flow test was conducted. In this test inverted slumpcone is filled with mortar slurry and lifted to a height of 1.0 m. The diameter of spread mortar occupied on plain surface is measured in two mutually perpendicular directions as shown in fig. 2. The average of these two is taken as the diameter of slump spread. For sufficient filling ability without bleeding and segregation required spread diameter should be between 350 mm to 380 mm. Flow test on fresh cement mortar to be used in casting SIFCON specimens were carried out with varying percentages of steel slag replacement.



Figure 2: Measurement of slump flow

5.2 Compressive strength test

The compressive strength was carried out as per IS 516:1959. The test was conducted on three cubes of size 100 x 100 x 100 mm for 7 and 28 days on compression testing machine.

5.3 Flexural strength test

Flexural test was carried out on prismatic specimens of size 100 x 100 x 500 mm using Universal Testing Machine as per IS 519:1959.

5.4 Split Tensile strength test

Split tension test was carried out on specimens of 100 mm diameter and 200mm height on compression testing machine as per IS 516:1959.

5.5 Impact Energy test

Impact Energy test was carried out on test specimens of 100 mm diameter and 50 mm height on impact testing machine, at 7 and 28 days. Drop weight type impact testing machine was used in accordance with method developed by Eren (1999). This machine (Fig. 3) is a combination of

aggregate impact value test machine and drop weight type test apparatus as recommended by ACI 544:1987.

The drop hammer for this test weighs 13.5 kg, and it is lifted and dropped from a height of 380 mm. Three cylinders were tested at 7 and 28 days age, and number of blows required to cause the first visible crack and ultimate failure was recorded.

First crack is defined as the first visible crack in the specimen under testing while the ultimate failure is reached when the cracks have opened up sufficiently to make the specimens touch each of the four positioning lugs at the base plate Fig.4 shows the specimens after failure by impact energy test.

Energy imparted to the specimen per blow is calculated by equation (1).

$$EI = \frac{1}{2} M V^2 N \tag{1}$$

Where;

EI = Impact energy (N-m),

M = Mass of drop hammer (kg),

V = Impact velocity = 1.8088 (m/s), and

N = Number of blows required for ultimate failure.

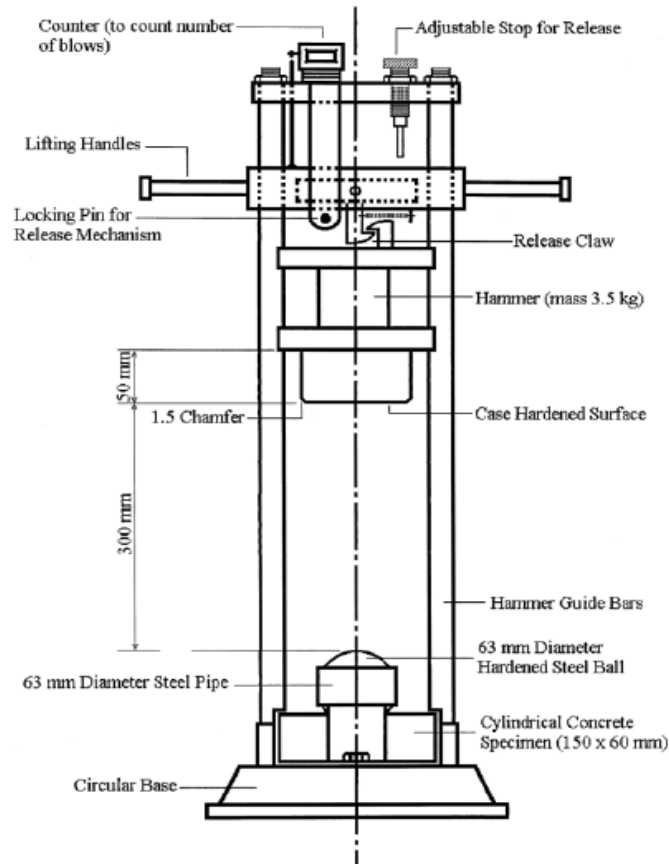


Figure 3: Assembly for Impact energy test



Figure 4: Impact Energy test specimen

6 Result and Discussion

The results of SIFCON for 2%, 3% and 4% fiber with 10% and 20% replacement of natural sand by steel slag are compared with the control mix having zero percentage of sand replacement and same fiber content. The results obtained from the study are shown in the Table 5 and subsequent discussion is presented as follows.

6.1 Compressive strength

1. Using 2%, 3% and 4% fiber by volume with 10 % replacement of sand by steel slag for 7 days compressive strength increased up to 2.95%, 13.22% and 14.28% respectively.
2. With 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 7 days compressive strength reduced up to 31.37%, 18.16% and 2.12% respectively.
3. Utilizing 2%, 3% and 4% fiber by volume with 10 % replacement of sand by steel slag for 28 days compressive strength increased up by 12.60%, 8.24% and 10.91% respectively.
4. Usage of 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 28 days compressive strength reduced up to 8.74%, 4.03% and 5.62% respectively.

6.2 Flexural strength

1. Using 2, 3 and 4% fiber by volume with 10 % replacement of sand by steel slag for 7 days Flexural strength increased up to 47.40%, 52.55% and 1.17% respectively.
2. With 2, 3 and 4% fiber by volume with 20 % replacement of sand by steel slag for 7 days Flexural strength increased up to 32.47%, 19.07% and 6.59 % respectively.
3. Utilizing 2%, 3% and 4% fiber by volume with 10 % replacement of sand by steel slag for 28 days Flexural strength increased up by 46.97%, 26.41% and 1.64% respectively.
4. Usage of 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 28 days Flexural strength increased up to 3.80%, 25.90% and 2.93% respectively.

Property	Fiber %	7 Day			28 Day		
		Control	10% slag	20% slag	Control	10% slag	20% slag
Compressive strength (Mpa)	2	31.83	32.77	24.23	44.05	49.60	40.20
	3	32.53	36.83	27.53	54.60	59.50	57.10
	4	35.57	39.80	34.83	63.80	70.76	60.40
Split tension strength (Mpa)	2	4.16	5.66	4.67	4.95	6.73	4.74
	3	5.14	5.68	5.60	7.11	7.23	6.62
	4	6.05	7.29	6.97	8.65	10.41	8.20
Flexural strength (Mpa)	2	7.30	10.76	9.67	9.75	14.33	10.12
	3	9.23	14.08	10.99	12.28	15.53	15.46
	4	15.32	15.50	16.33	18.08	18.29	18.61
Impact energy (N.m)	2	435.14	564.92	570.29	1368.02	1434.21	1456.28
	3	1106.94	2099.38	2129.85	1875.50	2909.83	3129.85
	4	2229.16	2340.13	2434.67	2329.35	3313.13	3343.67

Table 4: Test Results

6.3 Split tensile strength

1. Using 2%, 3% and 4% fiber by volume with 10 % replacement of sand by steel slag for 7 days Split tensile strength increased up to 36.06%, 1.43% and 20.50% respectively.
2. With 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 7 days Split tensile strength increased up to 10.90%, 4.16% and 6.04% respectively.
3. Utilizing 2%, 3% and 4% fiber by volume with 10 % replacement of sand by steel slag for 28 days Split tensile strength increased up by 40.00%, 1.69% and 20.35% respectively.
4. Usage of 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 28 days Split tensile strength reduced up to 4.20%, 6.89% and 5.20% respectively.

6.4 Impact Energy

1. Using 2%, 3% and 4% fiber by volume with 10 % replacement of sand by steel slag for 7 days Impact energy increased up to 29.83%, 89.66% and 4.98% respectively.
2. With 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 7 days Impact energy reduced up to 31.06%, 92.41% and 9.22% respectively.
3. With 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 28 days Impact energy reduced up to 4.84%, 55.15% and 42.23% respectively.

4. With 2%, 3% and 4% fiber by volume with 20 % replacement of sand by steel slag for 28 days Impact energy reduced up to 6.45%, 66.88% and 43.55% respectively.

From the above results, it is found that as the fiber content increases the strength parameters i.e. compressive strength, flexural strength and impact energy also increases. While discussing about the replacement level of the natural sand with steel slag, there is no reduction in strength found, rather the strength increases up to certain extent. 10% replacement is found to be optimum and gives the best results. The size of the steel slag used for the study is less than 2.00 mm, which fills the voids between sand particles and helps in improving the strength of concrete SIFCON. On a contrary if the replacement level is increased beyond optimum limit, it results in additional voids and becomes one of the reasons for strength reduction.

7 Failure Pattern

The failure pattern of conventional concrete and that of SIFCON specimens varies greatly. On one hand the failure of conventional concrete is brittle while on the other hand SIFCON shows ductile performance which is an added advantage of SIFCON. The failure of specimens under compression, split tension and flexure are shown in fig 5, fig 6 and fig 7 respectively and discussed below.

7.1 Failure of cubical specimen under compression

When compared to the standard control conventional concrete SIFCON displays failure after developing vertical cracks at edges, i.e. cup and cone formation.



Figure 5: Failure of cube specimen under compression

7.2 Failure of cylindrical specimen under compression in Split tensile strength test

SIFCON specimens' shows bulging while ordinary concrete shows splitting of specimen into two halves throughout.



Figure 6: Failure of cylindrical specimen under compression in split tensile strength test

7.3 Failure of beam specimen under Flexural strength test

On one hand when conventional concrete shows almost zero or negligible deflection, the SIFCON specimen shows exceptional ductile performance showing deflection of almost 7 mm. Further tests and experimentations show that as the age of concrete increases the deflection increases. As percentage of steel fiber increases the deflection also increases. This shows that the presence of steel fibers prevents the complete shear failure of beams. Diagonal cracks are formed below the point of application of load.



Figure 7: Failure of beam specimen under flexural tensile strength test

8 Conclusion

After the detailed experimentation and analysis of the result we have inferred that;

- SIFCON shows performance enhancement with lower percentages of steel fiber content by addition of additives such as steel slag. However, addition of steel slag reduces workability.
- An increase in the compressive, tensile, flexural and impact strength of SIFCON specimens were found in this study.

- Moreover, the 10% sand replacement was found to be optimum, except for the case of impact specimens where a direct relationship was observed between percentage replacement of steel slag and energy absorbed by specimen.
- When compared with control specimens of normal concrete the flexural behavior of SIFCON was observed to be more ductile.

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